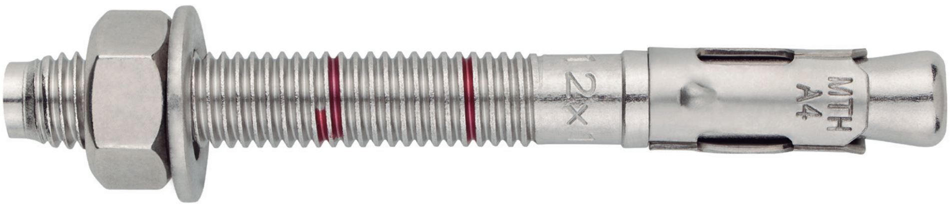
Through-bolt expansion anchor with controlled torque, for use in non cracked concrete

MTH-A4

ETA Assessed Option 7. A4 Stainless shaft. A4 Stainless clip.



PRODUCT INFORMATION

DESCRIPTION
Metallic anchor, with male thread, expansion by controlled torque.

OFFICIAL DOCUMENTATION
- AVCP-1219-CPR-0006.
- ETA 05/0242 Option 7.
- Declaration of Performance DoP MTH-A4
- MFPA Fire Protection Assessment.

SIZES
M6x45 to M20x220.

DESIGN LOAD RANGE
From 6,0 to 27,8 kN (standard depth).
From 5,0 to 8,9 kN (reduced depth).

BASE MATERIAL
Concrete class from C20/25 to C50/60 non-cracked.


Stone


Concrete


Reinforced concrete

ASSESSMENTS
- Option 7 (non-cracked concrete).

05
Técnicas Expansivas S.L.
Segador 13. Logroño. Spain
ETA 05/0242
1219
Structural fixings in non cracked concrete

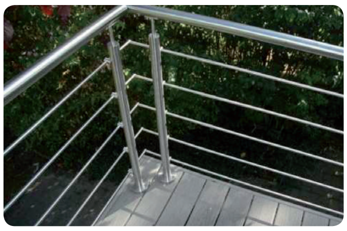
FIRE RESISTANCE

CHARACTERISTICS AND BENEFITS
- Easy installation.
- Use in non-craked concrete.
- Use for medium-heavy duty loads.
- Pre-installation or through the drill-hole of the fixture.
- Variety of lengths and diameters: flexibility in assembly.
- For static and quasi-static loads.
- Two installation depths in M8, M10 and M12 allowing the use in thick anchor plates or in los thickness base materials.
- Available at INDEXcal.
- Version in A4 Stainless steel (AISI 316).
- Available at INDEXcal.

MATERIALS
Shaft: A4 grade stainless steel.
Washer: A4 grade stainless steel.
Nut: A4 grade stainless steel.
Clip: AA4 grade stainless steel.

A4 INOX AISI 316

APPLICATIONS
- Coastal areas.
- Industrial areas.
- Food industries.
- Curtain walls.
- Fixings in tunnels.
- Pipe supports.
- Rehabilitation of facades.
- For outdoor use in general.



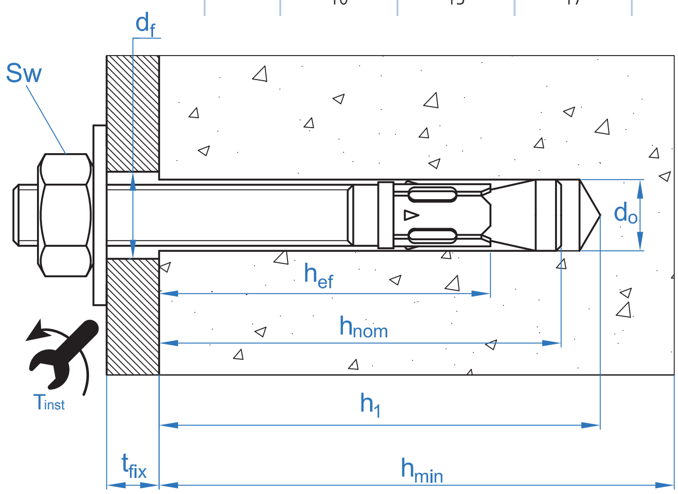
MECHANICAL PROPERTIES

			M6	M8	M10	M12	M16	M20
Cone area section								
A_s	(mm²)	Cone area section	14,5	27,3	49,0	70,9	122,7	201,1
$f_{u,s}$	(N/mm²)	Chracteristic tension resistance	700	700	700	700	700	700
$f_{y,s}$	(N/mm²)	Yield strength	500	500	500	500	500	500
Threaded area section								
A_s	(mm²)	Cone area section	20.1	36.6	58.0	84.3	157.0	245.0
$f_{u,s}$	(N/mm²)	Chracteristic tension resistance	600	600	600	600	600	600
$f_{y,s}$	(N/mm²)	Yield Strength	400	400	400	400	400	400

INSTALLATION DATA

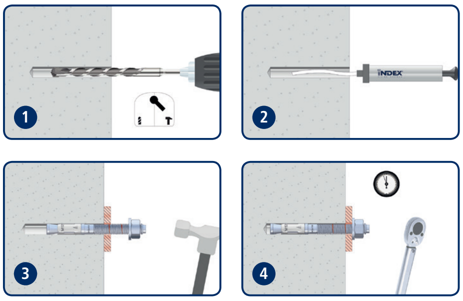
	SIZE			M6	M8	M10	M12	M16	M20
	Code			MIA406XXX	MIA408XXX	MIA410XXX	MIA412XXX	MIA416XXX	MIA420XXX
	d_0	Nominal diameter of drill bit	[mm]	6	8	10	12	16	20
	T_{ins}	Installation torque moment	[Nm]	7	20	35	60	120	240
	$d_f \leq$	Diameter of clearance hole in the fixture	[mm]	7	9	12	14	18	22
Standard depth	h_1	Minimum drill hole depth	[mm]	55	65	75	85	110	135
Standard depth	h_{nom}	Installation depth	[mm]	49,5	59,5	66,5	77	103,5	125
Standard depth	h_{ef}	Effective embedment depth	[mm]	40	48	55	65	84	103
Standard depth	h_{min}	Minimum base material thickness	[mm]	100	100	110	130	168	206
Standard depth	t_{fix}	Maximum thickness of fixture*	[mm]	L - 58	L - 70	L - 80	L - 92	L - 122	L - 147
Standard depth	$s_{cr,N}$	Critical spacing	[mm]	120	144	165	195	252	309
Standard depth	$c_{cr,N}$	Critical edge distance	[mm]	60	72	83	98	126	155
Standard depth	$s_{cr,sp}$	Critical distance (splitting)	[mm]	160	192	220	260	336	412
Standard depth	$c_{cr,sp}$	Critical edge distance (splitting)	[mm]	80	96	110	130	168	206
Reduced depth	h_1	Minimum drill hole depth	[mm]	-	50	60	70	-	-
Reduced depth	h_{nom}	Installation depth	[mm]	-	46,5	53,5	62	-	-
Reduced depth	h_{ef}	Effective embedment depth	[mm]	-	35	42	50	-	-
Reduced depth	h_{min}	Minimum base material thickness	[mm]	-	100	100	100	-	-
Reduced depth	t_{fix}	Maximum thickness of fixture*	[mm]	-	L-57	L-67	L-77	-	-
Reduced depth	$s_{cr,N}$	Critical spacing	[mm]	-	105	126	150	-	-
Reduced depth	$c_{cr,N}$	Critical edge distance	[mm]	-	53	63	75	-	-
Reduced depth	$s_{cr,sp}$	Critical distance (splitting)	[mm]	-	140	168	200	-	-
Reduced depth	$c_{cr,sp}$	Critical edge distance (splitting)	[mm]	-	70	84	100	-	-
	s_{min}	Minimum spacing	[mm]	50	65	70	85	110	135
	c_{min}	Minimum edge distance	[mm]	50	65	70	85	110	135
	SW	Installation wrench		10	13	17	19	24	30

*L = Total anchor length



Code	INSTALLATION PRODUCTS
	Hammer drill
BHDSXXXXX	Concrete Drill bits
MOBOMBA	Blow pump
MORCEPKIT	Cleaning Brush
DOMTAXX	Installation hammering tool
	Torque wrench
	Hexagonal socket

INSTALLATION



MTH-A4

Resistances in C20/25 concrete for an isolated anchor, without effects of edge distance or spacing

Characteristic Resistance N_{Rk} y V_{Rk}

TENSION

	Size		M6	M8	M10	M12	M16	M20
N_{Rk}	Standard depth	[kN]	10,1	12	16	25	35	50
N_{Rk}	Reduced depth	[kN]	-	9	12	16	-	-

SHEAR

	Size		M6	M8	M10	M12	M16	M20
V_{Rk}	Standard depth	[kN]	6,0	10,9	17,4	25,2	47,1	73,5
V_{Rk}	Reduced depth	[kN]	-	10,4	13,7	17,8	-	-

Design Resistance N_{Rd} y V_{Rd}

TENSION

	Size		M6	M8	M10	M12	M16	M20
N_{Rd}	Standard depth	[kN]	6,0	8,0	8,9	13,9	19,4	27,8
N_{Rd}	Reduced depth	[kN]	-	5,0	6,7	8,9	-	-

SHEAR

	Size		M6	M8	M10	M12	M16	M20
V_{Rd}	Standard depth	[kN]	3,9	7,1	11,4	16,6	30,1	48,3
V_{Rd}	Reduced depth	[kN]	-	7,0	9,1	11,9	-	-

Maximum Loads Recommended N_{rec} y V_{rec}

TENSION

	Size		M6	M8	M10	M12	M16	M20
N_{rec}	Standard depth	[kN]	4,3	5,7	6,3	9,9	13,9	19,8
N_{rec}	Reduced depth	[kN]	-	3,6	4,8	6,4	-	-

SHEAR

	Size		M6	M8	M10	M12	M16	M20
V_{rec}	Standard depth	[kN]	2,8	5,1	8,2	11,8	22,1	34,5
V_{rec}	Reduced depth	[kN]	-	4,9	6,5	8,5	-	-

Simplified calculation method

European Technical Assessment ETA 05/0242

Simplified version of the calculation method according to ETAG 001, annex C. Resistance is calculated according to the data shown in assessment ETA 05/0242.

- Influence of concrete strength.
- Influence of edge distance.
- Influence of spacing between anchors.
- Influence of reinforcements.
- Influence of base material thickness.
- Influence of load application angle.
- Valid for a group of two anchors.

The calculation method is based on the following simplification: **Different loads do not act on individual anchors, without eccentricity.**

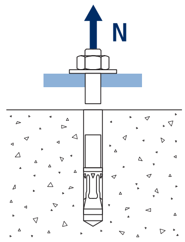
INDEXcal
For a more accurate calculation and to take more constructive provisions into account, we recommend using our calculation program INDEXcal. It may be easily downloaded from our website **www.indexfix.com**

MTH-A4

TENSION LOADS

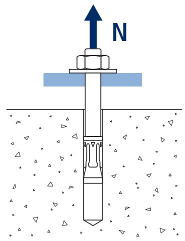
- Steel design resistance: $N_{Rd,s}$
- Pull-out design resistance: $N_{Rd,p} = N^o_{Rd,p} \cdot \Psi_c$
- Concrete cone design resistance: $N_{Rd,c} = N^o_{Rd,c} \cdot \Psi_b \cdot \Psi_{s,N} \cdot \Psi_{c,N} \cdot \Psi_{re,N}$
- Concrete splitting design resistance: $N_{Rd,sp} = N^o_{Rd,c} \cdot \Psi_b \cdot \Psi_{s,sp} \cdot \Psi_{c,sp} \cdot \Psi_{re,N} \cdot \Psi_{h,sp}$

Steel Design resistance								
$N_{Rd,s}$								
Size			M6	M8	M10	M12	M16	M20
N^o_{Rd}	Standard depth	[kN]	6,0	11,4	20,4	29,5	51,1	83,8



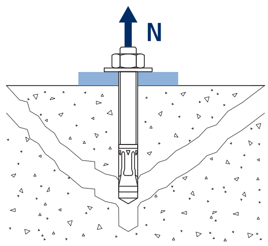
Pull-out design resistance								
$N_{Rd,p} = N^o_{Rd,p} \cdot \Psi_c$								
Size			M6	M8	M10	M12	M16	M20
$N^o_{Rd,p}$	Standard depth	[kN]	-*	8,0	8,9	13,9	19,4	27,8
$N^o_{Rd,p}$	Reduced depth	[kN]	-	5,0	6,7	8,9	-	-

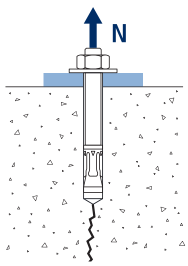
* Pull-out failure is not decisive.



Concrete cone design resistance								
$N_{Rd,c} = N^o_{Rd,c} \cdot \Psi_b \cdot \Psi_{s,N} \cdot \Psi_{c,N} \cdot \Psi_{re,N}$								
Concrete splitting design resistance*								
$N_{Rd,sp} = N^o_{Rd,c} \cdot \Psi_b \cdot \Psi_{s,sp} \cdot \Psi_{c,sp} \cdot \Psi_{re,N} \cdot \Psi_{h,sp}$								
Size			M6	M8	M10	M12	M16	M20
$N^o_{Rd,c}$	Standard depth	[kN]	8,5	11,2	11,4	14,7	21,6	29,3
$N^o_{Rd,c}$	Reduced depth	[kN]	-	5,8	7,6	9,9	-	-

*Concrete splitting design resistance must only be considered for non-cracked concrete.

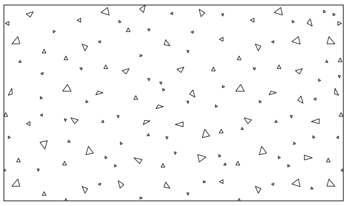




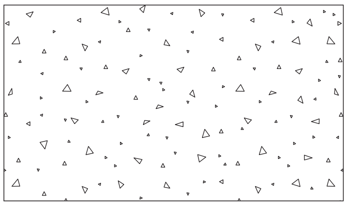
MTH-A4

Coefficients of influence

Influence of concrete strength resistance in pul-out failure Ψ_c							
		M6	M8	M10	M12	M16	M20
Ψ_c	C 20/25	1,00					
	C 30/37	1,22					
	C 40/50	1,41					
	C 50/60	1,55					

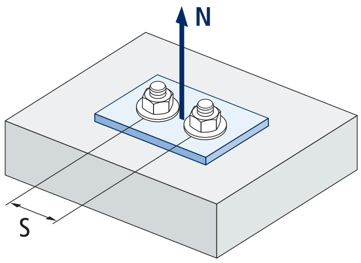


Influence of concrete strength in concrete cone and splitting failure Ψ_b							
		M6	M8	M10	M12	M16	M20
Ψ_b	C 20/25	1,00					
	C 30/37	1,22					
	C 40/50	1,41					
	C 50/60	1,55					



$$\Psi_b = \sqrt{\frac{f_{ck,cube}}{25}} \geq 1$$

MTH-A4



$$\Psi_{s,N} = 0,5 + \frac{S}{2 \cdot S_{cr,N}} \leq 1$$

Influence of spacing (concrete cone) $\Psi_{s,N}$

s [mm]	MTH-A4. Standard depth					
	M6	M8	M10	M12	M16	M20
50	0,71					
55	0,73					
60	0,75					
65	0,77	0,73				
70	0,79	0,74	0,71			
80	0,83	0,78	0,74			
85	0,85	0,80	0,76	0,72		
90	0,88	0,81	0,77	0,73		
100	0,92	0,85	0,80	0,76		
105	0,94	0,86	0,82	0,77		
110	0,96	0,88	0,83	0,78	0,72	
120	1,00	0,92	0,86	0,81	0,74	
125		0,93	0,88	0,82	0,75	
126		0,94	0,88	0,82	0,75	
128		0,94	0,89	0,83	0,75	
130		0,95	0,89	0,83	0,76	
135		0,97	0,91	0,85	0,77	0,72
144		1,00	0,94	0,87	0,79	0,73
150			0,95	0,88	0,80	0,74
165			1,00	0,92	0,83	0,77
170				0,94	0,84	0,78
180				0,96	0,86	0,79
195				1,00	0,89	0,82
200					0,90	0,82
210					0,92	0,84
220					0,94	0,86
225					0,95	0,86
252					1,00	0,91
255						0,91
260						0,92
300						0,99
309						1,00

Invalid value

Value without reduction = 1

s [mm]	MTH-A4. Reduced depth					
	M6	M8	M10	M12	M16	M20
65		0,81				
70		0,83	0,78			
80		0,88	0,82			
85		0,90	0,84	0,78		
90		0,93	0,86	0,80		
100		0,98	0,90	0,83		
105		1,00	0,92	0,85		
110			0,94	0,87		
120			0,98	0,90		
125			1,00	0,92		
126			1,00	0,92		
128				0,93		
130				0,93		
135				0,95		
144				0,98		
150				1,00		

Invalid value

Value without reduction = 1

MTH-A4

Influence of spacing (concrete splitting) $\Psi_{s,sp}$

s [mm]	MTH-A4. Standard depth					
	M6	M8	M10	M12	M16	M20
50	0,66					
55	0,67					
60	0,69					
65	0,70	0,67				
70	0,72	0,68	0,66			
80	0,75	0,71	0,68			
85	0,77	0,72	0,69	0,66		
90	0,78	0,73	0,70	0,67		
100	0,81	0,76	0,73	0,69		
110	0,84	0,79	0,75	0,71	0,66	
125	0,89	0,83	0,78	0,74	0,69	
128	0,90	0,83	0,79	0,75	0,69	
135	0,92	0,85	0,81	0,76	0,70	0,66
140	0,94	0,86	0,82	0,77	0,71	0,67
150	0,97	0,89	0,84	0,79	0,72	0,68
160	1,00	0,92	0,86	0,81	0,74	0,69
165		0,93	0,88	0,82	0,75	0,70
168		0,94	0,88	0,82	0,75	0,70
180		0,97	0,91	0,85	0,77	0,72
192		1,00	0,94	0,87	0,79	0,73
200			0,95	0,88	0,80	0,74
210			0,98	0,90	0,81	0,75
220			1,00	0,92	0,83	0,77
260				1,00	0,89	0,82
288					0,93	0,85
300					0,95	0,86
336					1,00	0,91
350						0,92
412						1,00

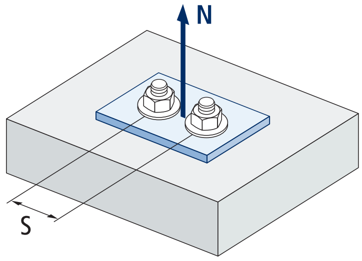
Invalid value (empty cells above the values)

Value without reduction = 1 (empty cells below the values)

s [mm]	MTH-A4. Reduced depth					
	M6	M8	M10	M12	M16	M20
65		0,73				
70		0,75	0,71			
80		0,79	0,74			
85		0,80	0,75	0,71		
90		0,82	0,77	0,73		
100		0,86	0,80	0,75		
110		0,89	0,83	0,78		
125		0,95	0,87	0,81		
128		0,96	0,88	0,82		
135		0,98	0,90	0,84		
140		1,00	0,92	0,85		
150			0,95	0,88		
160			0,98	0,90		
165			0,99	0,91		
168			1,00	0,92		
180				0,95		
192				0,98		
200				1,00		

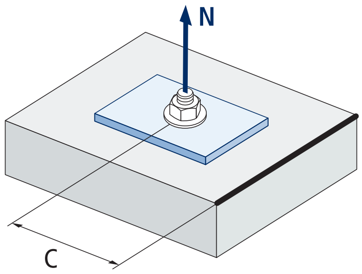
Invalid value (M6 column blank; M16 and M20 columns and empty cells above the values)

Value without reduction = 1 (empty cells below the values)



$$\Psi_{s,sp} = 0{,}5 + \frac{s}{2 \cdot s_{cr,sp}} \leq 1$$

MTH-A4



$$\Psi_{c,sp} = 0,35 + \frac{0,5 \cdot c}{C_{cr,sp}} + \frac{0,15 \cdot c^2}{C_{cr,sp}^{\,2}} \le 1$$

Influence of concrete edge distance (splitting) $\Psi_{c,sp}$

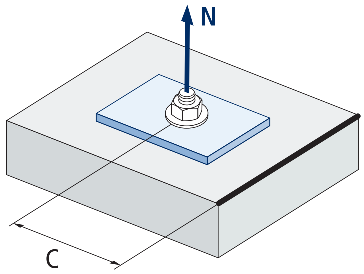
c [mm]	**MTH-A4.** Standard depth					
	M6	M8	M10	M12	M16	M20
50	0,72					
60	0,81					
65	0,86	0,76			**Invalid value**	
70	0,90	0,79	0,73			
75	0,95	0,83	0,76			
80	1,00	0,87	0,79			
83		0,89	0,81			
84		0,90	0,82			
85		0,91	0,83	0,74		
90		0,95	0,86	0,77		
96		1,00	0,90	0,80		
100			0,93	0,82		
105			0,96	0,85		
110			1,00	0,88	0,74	
125				0,97	0,81	
128				0,99	0,82	
130				1,00	0,83	
135					0,85	0,74
144					0,89	0,77
150					0,92	0,79
168					1,00	0,86
175			**Value without reduction = 1**			0,88
180						0,90
206						1,00

c [mm]	**MTH-A4.** Reduced depth					
	M6	M8	M10	M12	M16	M20
50		0,78				
60		0,89	0,78			
65		0,94	0,83		**Invalid value**	
70		1,00	0,87			
75			0,92			
80			0,96			
83			0,99	0,87		
84			1,00	0,88		
85				0,88		
90		**Value without reduction = 1**		0,92		
96				0,97		
100				1,00		

MTH-A4

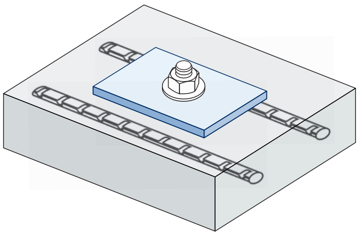
Influence of concrete edge distance (concrete cone) $\Psi_{c,N}$						
c [mm]	**MTH-A4.** Standard depth					
	M6	M8	M10	M12	M16	M20
50	0,87					
53	0,91					
60	1,00				**Invalid value**	
63						
65		0,92				
70		0,98	0,88			
72		1,00	0,90			
75			0,92			
80			0,97			
83			1,00			
85				0,90		
90				0,94		
98				1,00		
100						
105						
110					0,90	
113					0,92	
125					0,99	
126					1,00	
128						
135		**Value without reduction = 1**				0,90
150						0,97
155						1,00

c [mm]	**MTH-A4.** Reduced depth					
	M6	M8	M10	M12	M16	M20
65		1,00				
70			1,00			
72					**Invalid value**	
75						
80		**Value without reduction = 1**				
83						
85				1,00		



$$\Psi_{c,N} = 0{,}35 + \frac{0{,}5 \cdot c}{C_{cr,N}} + \frac{0{,}15 \cdot c^2}{C_{cr,N}^{\ 2}} \leq 1$$

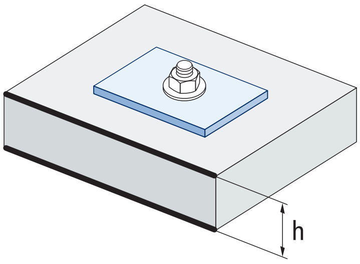
MTH-A4



$$\Psi_{re,N} = 0,5 + \frac{h_{ef}}{200} \le 1$$

Influence of reinforcements $\Psi_{re,N}$						
	MTH-A4. Standard depth					
	M6	M8	M10	M12	M16	M20
$\Psi_{re,N}$	0,70	0,74	0,77	0,82	0,92	1,00
	MTH-A4. Reduced depth					
	M6	M8	M10	M12	M16	M20
$\Psi_{re,N}$	-	0,67	0,71	0,75	-	-

*This factor only applies for a high density of reinforcements. If in the area of the anchor there are reinforcements with a distancing of ≥ 150 mm (any diameter) or with a diameter ≤ 10 mm and a distancing of ≥ 100 mm, a $f_{re,N}$ = 1 factor may be applied.



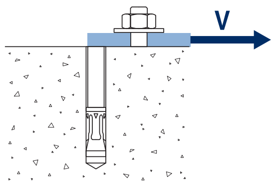
Influence of base material thickness $\Psi_{h,sp}$											
	MTH-A4										
$\Psi_{h,sp}$	h/hef	2,00	2,20	2,40	2,60	2,80	3,00	3,20	3,40	3,60	≥3,68
	$\Psi_{h,sp}$	1,00	1,07	1,13	1,19	1,25	1,31	1,37	1,42	1,48	1,50

$$\Psi_{h,sp} = \left(\frac{h}{2 \cdot h_{ef}}\right)^{2/3} \le 1,5$$

SHEAR LOADS

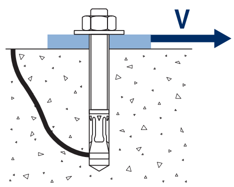
- Steel design resistance without lever arm: $V_{Rd,s}$
- Pry-out design resistance: $V_{Rd,cp} = k \cdot N^{o}_{Rd,c}$
- Concrete edge design resistance: $V_{Rd,c} = V^{o}_{Rd,c} \cdot \Psi_{b} \cdot \Psi_{se,V} \cdot \Psi_{c,V} \cdot \Psi_{re,V} \cdot \Psi_{\alpha,V} \cdot \Psi_{h,V}$

Steel design resistance								
$V_{Rd,s}$								
Size			M6	M8	M10	M12	M16	M20
$V_{Rd,s}$	Standard depth	[kN]	3,9	7,2	11,4	16,6	31,0	48,4
$V_{Rd,s}$	Reduced depth	[kN]	-	7,2	11,4	16,6	-	-

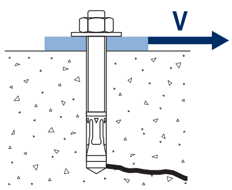


Pry-out design resistance*						
$V_{Rd,cp} = k \cdot N^{o}_{Rd,c}$						
Size	M6	M8	M10	M12	M16	M20
k (Standard depth)	1	1	1	2	2	2
k (Reduced depth)	-	1	1	1	-	-

* $N^{o}_{Rd,c}$ Concrete cone design resistance for tension loads



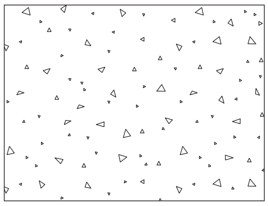
Concrete edge resistance								
$V_{Rd,c} = V^{o}_{Rd,c} \cdot \Psi_{b} \cdot \Psi_{se,V} \cdot \Psi_{c,V} \cdot \Psi_{re,V} \cdot \Psi_{\alpha,V} \cdot \Psi_{h,V}$								
Size			M6	M8	M10	M12	M16	M20
$V^{o}_{Rd,c}$	Standard depth	[kN]	4,6	6,2	7,7	10,2	15,6	21,8
$V^{o}_{Rd,c}$	Reduced depth	[kN]	-	3,7	4,9	6,6	-	-



MTH-A4

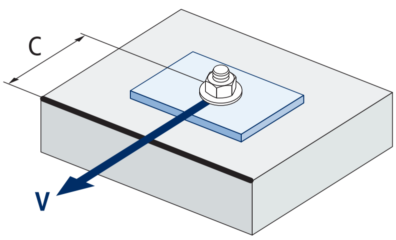
Coefficients of influence

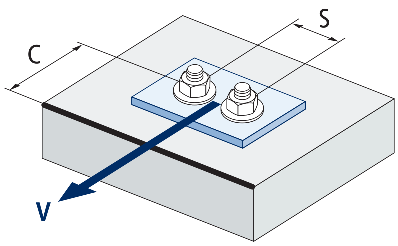
Influence of concrete strength in concrete edge failure Ψ_b							
		M6	M8	M10	M12	M16	M20
Ψ_b	C 20/25	1,00					
	C 30/37	1,22					
	C 40/50	1,41					
	C 50/60	1,55					



$$\Psi_b = \sqrt{\frac{f_{ck,cube}}{25}} \geq 1$$

Influence of edge distance and spacing $\Psi_{se,V}$																		
FOR ONE ANCHOR ONLY																		
	c/h_{ef}	0,50	0,75	1,00	1,25	1,50	1,75	2,00	2,25	2,50	2,75	3,00	3,25	3,50	3,75	4,00	4,50	5,00
	Isolated	0,35	0,65	1,00	1,40	1,84	2,32	2,83	3,38	3,95	4,56	5,20	5,86	6,55	7,26	8,00	9,55	11,18
FOR TWO ANCHORS																		
	c/h_{ef}	0,50	0,75	1,00	1,25	1,50	1,75	2,00	2,25	2,50	2,75	3,00	3,25	3,50	3,75	4,00	4,50	5,00
s/c	1,0	0,24	0,43	0,67	0,93	1,22	1,54	1,89	2,25	2,64	3,04	3,46	3,91	4,37	4,84	5,33	6,36	7,45
	1,5	0,27	0,49	0,75	1,05	1,38	1,74	2,12	2,53	2,96	3,42	3,90	4,39	4,91	5,45	6,00	7,16	8,39
	2,0	0,29	0,54	0,83	1,16	1,53	1,93	2,36	2,81	3,29	3,80	4,33	4,88	5,46	6,05	6,67	7,95	9,32
	2,5	0,32	0,60	0,92	1,28	1,68	2,12	2,59	3,09	3,62	4,18	4,76	5,37	6,00	6,66	7,33	8,75	10,25
	≥3,0	0,35	0,65	1,00	1,40	1,84	2,32	2,83	3,38	3,95	4,56	5,20	5,86	6,55	7,26	8,00	9,55	11,18

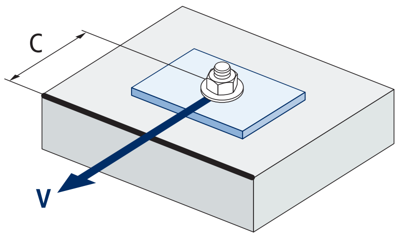




$$\Psi_{se,V} = \left(\frac{c}{h_{ef}}\right)^{1,5}$$

$$\Psi_{se,V} = \left(\frac{c}{h_{ef}}\right)^{1,5} \cdot \left(1 + \frac{s}{3 \cdot c}\right) \cdot 0,5 \leq \left(\frac{c}{h_{ef}}\right)^{1,5}$$

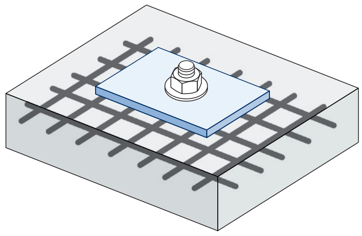
MTH-A4



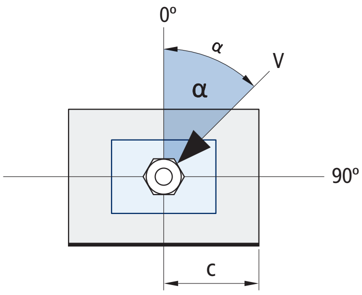
$$\Psi_{c,V} = \left(\frac{d}{c}\right)^{0,20}$$

Influence of concrete edge distance $\Psi_{c,V}$						
c [mm]	MTH-A4					
	M6	M10	M10	M12	M16	M20
40						
45						
50	0,65					
55	0,64			Invalid value		
60	0,63					
65	0,62	0,66				
70	0,61	0,65	0,68			
80	0,60	0,63	0,66			
85	0,59	0,62	0,65	0,68		
90	0,58	0,62	0,64	0,67		
100	0,57	0,60	0,63	0,65	0,67	
105	0,56	0,60	0,62	0,65	0,67	
110	0,56	0,59	0,62	0,64	0,66	0,68
120	0,55	0,58	0,61	0,63	0,65	0,67
125	0,54	0,58	0,60	0,63	0,65	0,66
130	0,54	0,57	0,60	0,62	0,64	0,66
135	0,54	0,57	0,59	0,62	0,64	0,65
140	0,53	0,56	0,59	0,61	0,63	0,65
150	0,53	0,56	0,58	0,60	0,62	0,64
160	0,52	0,55	0,57	0,60	0,61	0,63
170	0,51	0,54	0,57	0,59	0,61	0,62
175	0,51	0,54	0,56	0,59	0,60	0,62
180	0,51	0,54	0,56	0,58	0,60	0,62
190	0,50	0,53	0,55	0,58	0,59	0,61
200	0,50	0,53	0,55	0,57	0,59	0,60
210	0,49	0,52	0,54	0,56	0,58	0,60
220	0,49	0,52	0,54	0,56	0,58	0,59
230	0,48	0,51	0,53	0,55	0,57	0,59
240	0,48	0,51	0,53	0,55	0,57	0,58
250	0,47	0,50	0,53	0,54	0,56	0,58
260	0,47	0,50	0,52	0,54	0,56	0,57
270	0,47	0,49	0,52	0,54	0,55	0,57
280	0,46	0,49	0,51	0,53	0,55	0,56
290	0,46	0,49	0,51	0,53	0,55	0,56
300	0,46	0,48	0,51	0,53	0,54	0,56

Influence of reinforcements $\Psi_{re,V}$			
	Without perimetral reinforcements	Perimetral reinforcements ≥ Ø12 mm	Perimetral reinforcements with brackets ≤ 100 mm
Non-cracked concrete	1	1	1

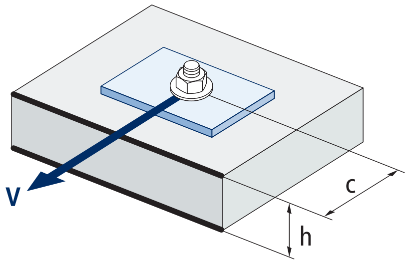


Influence of load application angle $\Psi_{\alpha,V}$										
Angle, α(º)	0º	10º	20º	30º	40º	50º	60º	70º	80º	90º
$\Psi_{\alpha,V}$	1,00	1,01	1,05	1,13	1,24	1,40	1,64	1,97	2,32	2,50



$$\Psi_{\alpha,V} = \sqrt{\frac{1}{(\cos \alpha_V)^2 + \left(\frac{\sin \alpha_V}{2,5}\right)^2}} \geq 1$$

Influence of base material thickness $\Psi_{h,V}$										
MTH-A4										
h/c	0,15	0,30	0,45	0,60	0,75	0,90	1,05	1,20	1,35	≥1,5
$\Psi_{h,V}$	0,32	0,45	0,55	0,63	0,71	0,77	0,84	0,89	0,95	1,00



$$\Psi_{h,V} = \left(\frac{h}{1,5 \cdot c}\right)^{0,5} \geq 1,0$$

MTH-A4

FIRE RESISTANCE

Characteristic Resistance*												
	TENSION						SHEAR					
	M6	M8	M10	M12	M16	M20	M6	M8	M10	M12	M16	M20
RF30	-	0,8	1,5	2,4	4,5	7,0	-	0,8	1,5	2,4	4,5	7,0
RF60	-	0,7	1,2	2,0	3,6	5,7	-	0,7	1,2	2,0	3,6	5,7
RF90	-	0,5	1,0	1,5	2,7	4,3	-	0,5	1,0	1,5	2,7	4,3
RF120	-	0,5	0,8	1,2	2,3	3,6	-	0,5	0,8	1,2	2,3	3,6

*The safety factor for design resistance under fire exposure is $\gamma_{M,fi}$=1 (in abscence of other national regulations). As a eresult the Characteristic Resistance is the same as Design Resistance.

Maximum Load Recommended												
	TENSION						SHEAR					
	M6	M8	M10	M12	M16	M20	M6	M8	M10	M12	M16	M20
RF30	-	0,6	1,1	1,7	3,2	5,0	-	0,6	1,1	1,7	3,2	5,0
RF60	-	0,5	0,9	1,4	2,6	4,0	-	0,5	0,9	1,4	2,6	4,0
RF90	-	0,4	0,7	1,1	2,0	3,1	-	0,4	0,7	1,1	2,0	3,1
RF120	-	0,3	0,6	0,9	1,6	2,6	-	0,3	0,6	0,9	1,6	2,6

• Fire resitance values are not covered by ETA.

RANGE

Code	Size	Maximum thickness of fixture	Axle letter (length)		
• MIA406045	M6 x 45 Ø6	1	A	200	1.200
MIA406060	M6 x 60 Ø6	2	B	200	1.200
MIA406080	M6 x 80 Ø6	22	D	200	1.200
• MIA408050	M8 x 50 Ø8	4	A	100	800
MIA408075	M8 x 75 Ø8	5	C	100	600
MIA408090	M8 x 90 Ø8	20	E	100	600
MIA408115	M8 x 115 Ø8	45	G	100	400
MIA410070	M10 x 70 Ø10	3	C	100	400
MIA410090	M10 x 90 Ø10	10	D	100	400
MIA410120	M10 x 120 Ø10	40	G	50	300
MIA410150	M10 x 150 Ø10	70	I	50	200

Code	Size	Maximum thickness of fixture	Axle letter (length)		
• MIA412075	M12 x 75 Ø12	5	C	50	300
MIA412090	M12 x 90 Ø12	13	D	50	200
MIA412110	M12 x 110 Ø12	12	F	50	200
MIA412140	M12 x 140 Ø12	42	I	50	200
• MIA416090	M16 x 90 Ø16	4	D	25	150
MIA416145	M16 x 145 Ø16	23	I	25	100
MIA416170	M16 x 170 Ø16	48	K	25	75
• MIA420120	M20 x 120 Ø20	5	G	20	80
MIA420170	M20 x 170 Ø20	23	K	20	80
MIA420220	M20 x 220 Ø20	73	O	20	60

• Non assessed sizes. Resistance values and installation data are not applicable to these references. For further information, please contact Technical Department.